

Reduced order methods for optimal flow control problems

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Abstract

We propose a reduced basis (RB) framework for the numerical solution of optimal control problems for parametrized viscous incompressible flows. We mainly focus on control problems for the (Navier-) Stokes equations involving infinitedimensional control functions, thus requiring a suitable reduction of the whole optimization problem, rather than of the sole state equation. The method is applied to the solution of a data assimilation problem arising in haemodynamics and a problem of vorticity minimization through suction/injection of fluid. The stability of the RB approximation can be fulfilled by introducing suitable supremizer solutions [5] and by defining suitable *aggregated spaces* for the state and adjoint variables [6]. The reduced basis approximation reads:

given $\boldsymbol{\mu} \in \mathcal{D}$, find $(x_N(\boldsymbol{\mu}), p_N(\boldsymbol{\mu})) \in X_N \times Q_N$ such that

 $\begin{cases} \mathcal{J}_{X}(x_{N}(\boldsymbol{\mu});\boldsymbol{\mu}) + \mathcal{E}_{X}(x_{N}(\boldsymbol{\mu});\boldsymbol{\mu})^{*}p_{N}(\boldsymbol{\mu}) &= 0, & \text{in } X_{N}' \\ \mathcal{E}(x_{N}(\boldsymbol{\mu});\boldsymbol{\mu}) &= 0, & \text{in } Q_{N}', \end{cases}$

5. Navier-Stokes constraint: main ingredients

In this case, the optimality system (5) forms a non-linear system to which we can apply Newton's method: for $k = 1, 2, ..., \text{ seek } (s_x^k, s_p^k) \in X \times Q$ such that

 $\begin{cases} \mathcal{L}_{XX}(x^k, p^k; \boldsymbol{\mu}) s_X^k + \mathcal{E}_X(x^k; \boldsymbol{\mu})^* s_p^k = -\mathcal{L}_X(x^k, p^k; \boldsymbol{\mu}), \\ \mathcal{E}(x^k, \boldsymbol{\mu}) s_X^k + \mathcal{E}_X(x^k; \boldsymbol{\mu})^* s_p^k = -\mathcal{E}(x^k, \boldsymbol{\mu}), \end{cases}$



1. Problem definition

We consider the following parametrized optimal control problem:

given $\mu \in \mathcal{D}$, find a triple $(\mathbf{v}, \pi, \mathbf{u})$ such that the cost functional

$$\mathcal{J}(\mathbf{v},\pi,\mathbf{u};oldsymbol{\mu})=\mathcal{F}(\mathbf{v},\pi;oldsymbol{\mu})+\mathcal{G}(\mathbf{u};oldsymbol{\mu})$$

(1)

is minimized subject to the steady (Navier-)Stokes equations:

$$-\nu \Delta \mathbf{v} + \delta(\mathbf{v} \cdot \nabla) \mathbf{v} + \pi = \mathbf{0} \qquad \text{in } \Omega_o(\boldsymbol{\mu})$$

$$\operatorname{div} \mathbf{v} = 0 \qquad \text{in } \Omega_o(\boldsymbol{\mu})$$

$$\mathbf{v} = \rho_1 \mathbf{u}_1 \qquad \text{on } \Gamma_D^o(\boldsymbol{\mu})$$

$$-\pi \mathbf{n} + \nu \nabla \mathbf{v} \cdot \mathbf{n} = \rho_2 \mathbf{u}_2 \qquad \text{on } \Gamma_N^o(\boldsymbol{\mu}).$$
(2)

Here $\Omega_o(\boldsymbol{\mu}) \subset \mathbb{R}^2$ is a parametrized domain with boundary $\partial \Omega_o = \Gamma_D^o \cup \Gamma_N^o$, being Γ_D^o the Dirichlet portion of the boundary and Γ_N^o the Neumann portion. The PDE constraint is given by the Navier-Stokes (Stokes) equations if $\delta = 1$ $(\delta = 0)$; the state variables \mathbf{v} and π denote the velocity and pressure fields, respectively. The boolean variables ρ_i satisfy $\rho_1 + \rho_2 = 1$, so that the control variable \mathbf{u} may represent

3. Stokes constraint: main ingredients

Since the cost functional is quadratic and the state equation is linear, the optimality system is linear and features a saddlepoint structure. At the algebraic level we obtain the linear system

$$\underbrace{\begin{pmatrix} A_{N}(\boldsymbol{\mu}) & B_{N}^{T}(\boldsymbol{\mu}) \\ B_{N}(\boldsymbol{\mu}) & 0 \end{pmatrix}}_{\mathcal{K}_{N}(\boldsymbol{\mu})} \begin{pmatrix} \mathbf{x}_{N}(\boldsymbol{\mu}) \\ \mathbf{p}_{N}(\boldsymbol{\mu}) \end{pmatrix} = \underbrace{\begin{pmatrix} \mathbf{F}_{N}(\boldsymbol{\mu}) \\ \mathbf{G}_{N}(\boldsymbol{\mu}) \end{pmatrix}}_{\mathbf{f}_{N}(\boldsymbol{\mu})}.$$
 (6)
Thanks to the affine assumption, we can write
$$\mathcal{K}_{N}(\boldsymbol{\mu}) = \sum_{q=1}^{Q_{k}} \Theta_{k}^{q}(\boldsymbol{\mu}) \mathcal{K}_{N}^{q}, \qquad \mathbf{f}_{N}(\boldsymbol{\mu}) = \sum_{q=1}^{Q_{f}} \Theta_{f}^{q}(\boldsymbol{\mu}) f_{N}^{q},$$

where K_N^q and f_N^q are μ -independent, and we can therefore provide the usual Offline-Online computational decomposition.

Recasting the problem in the general Babuška framework [5] we can provide an efficient and rigorous a posteriori error estimate on the solution variables (as well as on the cost functional [4]):

 $\|(x_h(\boldsymbol{\mu}), p_h(\boldsymbol{\mu})) - (x_N(\boldsymbol{\mu}), p_N(\boldsymbol{\mu}))\|_{X \times Q} \leq \frac{\|\mathbf{r}(\cdot; \boldsymbol{\mu})\|}{\beta_{LB}(\boldsymbol{\mu})} = \Delta_N(\boldsymbol{\mu})$ where $0 < \beta_{LB}(\boldsymbol{\mu}) \leq \beta_h(\boldsymbol{\mu})$ is a *lower bound* of the inf-sup constant of the optimality system. $\int \mathcal{E}(x^k;\boldsymbol{\mu})s_x^k = -\mathcal{E}(x^k;\boldsymbol{\mu}),$

and then set $(x^{k+1}, p^{k+1}) = (x^k, p^k) + (s_x^k, s_p^k)$. The main ingredients of our reduction strategy are the following:

- in the Online stage we solve the reduced optimization problem by first projecting the optimality system on the RB spaces and then applying Newton's method;
- the Offline/Online computational stratagem is preserved thanks to the quadratic nature of the nonlinear terms appearing in both first and second order derivatives;
- in order to derive an posteriori error estimate on the state, adjoint and control variables, we apply the Brezzi-Rappaz-Raviart theory on the optimality system.

6. Vorticity minimization past a bluff body

As a preliminary benchmark test, we consider the problem of vorticity minimization through suction/injection of fluid in the downstream portion of a bluff body embedded in a 2-D flow. In this case we do not consider a geometrical parametrization, yet we take as parameters the Reynolds number and the regularization constant in the cost functional. In the figures below we show the convergence of the RB approximation, a comparison between an uncontrolled and a controlled flow, and the value of the cost functional with respect to the parameters.

either a boundary velocity on $\Gamma_D^o(\mathbf{u}_1)$ or a Neumann flux on $\Gamma_N^o(\mathbf{u}_2)$. $\mathcal{F}(\mathbf{v}, \pi; \boldsymbol{\mu})$ represents the objective to be minimized, while $\mathcal{G}(\mathbf{u}; \boldsymbol{\mu})$ is a regularization term ensuring the well-posedness of the problem. Possible choices for \mathcal{F} are the viscous energy dissipation and vorticity type functionals or velocity tracking type functionals.

The optimal control problem (1)-(2) can be formulated in the following general form [2]: given $\mu \in \mathcal{D}$,

 $\min_{x \in X_o} \mathcal{J}_o(x; \boldsymbol{\mu}) \quad \text{s.t.} \quad \mathcal{E}_o(x) = 0 \quad \text{in } X'_o, \tag{3}$

where X_o and Q_o are two Hilbert spaces, $x = (\mathbf{v}, \pi, \mathbf{u}) \in X_o$ is the optimization variable and the operator $\mathcal{E}_o \colon X_o \to Q'_o$ describes the state equation. We assume that the original domain $\Omega_o(\boldsymbol{\mu})$ can be obtained as the image of a reference (parameter independent) domain $\Omega = \Omega_o(\boldsymbol{\mu}_{ref})$ through a (affine or nonaffine) parametrized mapping $T(\cdot; \boldsymbol{\mu}) \colon \mathbb{R}^2 \times \mathcal{D} \to \mathbb{R}^2$. The parametrized formulation of the optimal control problem can be derived by tracing (3) back on the reference domain Ω [6]:

given
$$\boldsymbol{\mu} \in \mathcal{D}$$
, $\min_{x \in X} \mathcal{J}(x; \boldsymbol{\mu})$ s.t. $\mathcal{E}(x; \boldsymbol{\mu}) = 0$, (4)

where the cost functional and the state operator are linked to the "original" ones through the mapping $T(\cdot; \mu)$.

By introducing the Lagrangian functional $\mathcal{L}(x, p; \boldsymbol{\mu}) = \mathcal{J}(x; \boldsymbol{\mu}) + \langle \mathcal{E}(x; \boldsymbol{\mu}), p \rangle$, we can derive the first order necessary optimality conditions:

4. A boundary inverse problem

We consider an inverse boundary problem in haemodynamics (inspired by the work in [1]) where the state equation models the blood flow (supposed to obey the Stokes equations) in a parametrized arterial bifurcation and we suppose to have a measured velocity profile on the a transverse section, but not the Neumann flux on Γ_C that will be our control variable.



With respect to the formulation (1)-(2) we consider a Neumann control (thus $\rho_2 = 1$) and the following cost functional

$$\mathcal{J}(\boldsymbol{v}, \boldsymbol{\pi}; \boldsymbol{u}; \boldsymbol{\mu}) = \frac{1}{2} \int_{\Gamma_{obs}} |\boldsymbol{v} - \boldsymbol{v}_d(\boldsymbol{\mu}_{obs})|^2 d\Gamma + \frac{\alpha_1}{2} \int_{\Gamma_c} |\nabla \mathbf{u}|^2 d\Gamma + \frac{\alpha_2}{2} \int_{\Gamma_c} |\mathbf{u}|^2 d\Gamma.$$

• Geometrical parametrization: Free Form Deformation the geometrical parameter μ_q is related to the angle of





Uncontrolled (left) vs controlled (right) flow.



References

 $\begin{cases} \mathcal{J}_{X}(x;\boldsymbol{\mu}) + \mathcal{E}_{X}(x;\boldsymbol{\mu})^{*}p &= 0, & \text{in } X' \\ \mathcal{E}(x;\boldsymbol{\mu}) &= 0, & \text{in } Q', \end{cases}$ (5)

being $p(\mu) \in Q$ the Lagrange multiplier (adjoint variable) associated to the constraint.

2. Reduced basis approximation

The RB method gives an efficient way to compute an approximation to the FE *truth* solution $(x_h(\boldsymbol{\mu}), p_h(\boldsymbol{\mu}))$ by considering only a small subspace of the FE space $X_h \times Q_h$. We thus take a suitably selected (by a greedy algorithm) set of parameter values $\boldsymbol{\mu}^1, \ldots, \boldsymbol{\mu}^N$ ($N \ll N_h$) and the corresponding FE solutions $(x_h(\boldsymbol{\mu}^1), p_h(\boldsymbol{\mu}^1)), \ldots, (x_h(\boldsymbol{\mu}^N), p_h(\boldsymbol{\mu}^N))$.

rotation of the lower branch.

• Parametrized measured velocity profiles:





Examples of reconstructed velocity fields

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