

Supplementary material for the article
*Tunable morphing of electroactive dielectric-elastomer
 balloons*

Yipin Su^{1,*}, Davide Riccobelli^{1,*}, Yingjie Chen^{2,*},
 Weiqiu Chen^{2,3}, Pasquale Ciarletta¹

¹ MOX – Dipartimento di Matematica, Politecnico di Milano,
 Piazza Leonardo da Vinci 32, Milan 20133, Italy

² Department of Engineering Mechanics, Zhejiang University,
 Hangzhou 310027, PR China

³Shenzhen Research Institute of Zhejiang University,
 Shenzhen 518057, PR China

* These authors equally contributed to the work.

1 Derivation of the Stroh formulation

The incremental constitutive relation can be obtained by expanding Eq. (3.1), as

$$\begin{aligned}
 \dot{S}_{\theta r} &= A_{2121} \frac{1}{r} \frac{\partial \dot{u}_r}{\partial \theta} - A_{2121} \frac{\dot{u}_\theta}{r} + (A_{1221} + p) \frac{\partial \dot{u}_\theta}{\partial r} + \Gamma_{122} \dot{D}_\theta, \\
 \dot{S}_{\theta\theta} &= A_{1122} \frac{\partial \dot{u}_r}{\partial r} + (A_{2222} + p) \frac{1}{r} \left(\dot{u}_r + \frac{\partial \dot{u}_\theta}{\partial \theta} \right) + A_{2233} \frac{1}{r} (\dot{u}_r + \dot{u}_\theta \cot \theta) + \Gamma_{221} \dot{D}_r - \dot{p}, \\
 \dot{S}_{\psi\psi} &= A_{1122} \frac{\partial \dot{u}_r}{\partial r} + A_{2233} \frac{1}{r} \left(\dot{u}_r + \frac{\partial \dot{u}_\theta}{\partial \theta} \right) + (A_{2222} + p) \frac{1}{r} (\dot{u}_r + \dot{u}_\theta \cot \theta) + \Gamma_{221} \dot{D}_r - \dot{p}, \\
 \dot{S}_{r\theta} &= A_{1212} \frac{\partial \dot{u}_\theta}{\partial r} + (A_{1221} + p) \frac{1}{r} \frac{\partial \dot{u}_r}{\partial \theta} - (A_{1221} + p) \frac{\dot{u}_\theta}{r} + \Gamma_{122} \dot{D}_\theta, \\
 \dot{S}_{\theta r} &= A_{2121} \frac{1}{r} \frac{\partial \dot{u}_r}{\partial \theta} - A_{2121} \frac{\dot{u}_\theta}{r} + (A_{1221} + p) \frac{\partial \dot{u}_\theta}{\partial r} + \Gamma_{122} \dot{D}_\theta, \\
 \dot{E}_r &= -\frac{\partial \dot{\phi}}{\partial r} = \Gamma_{111} \frac{\partial \dot{u}_r}{\partial r} + \Gamma_{221} \left[\frac{1}{r} \left(\dot{u}_r + \frac{\partial \dot{u}_\theta}{\partial \theta} \right) + \frac{1}{r} (\dot{u}_r + \dot{u}_\theta \cot \theta) \right] + K_{011} \dot{D}_r, \\
 \dot{E}_\theta &= -\frac{1}{r} \frac{\partial \dot{\phi}}{\partial \theta} = \Gamma_{122} \left[\frac{\partial \dot{u}_\theta}{\partial r} + \frac{1}{r} \left(\frac{\partial \dot{u}_r}{\partial \theta} - \dot{u}_\theta \right) \right] + K_{22} \dot{D}_\theta.
 \end{aligned} \tag{S1}$$

The components of the incremental equilibrium equation (3.3) and the incremental Maxwell equation (3.5) read

$$\begin{aligned}
 \frac{\partial \dot{S}_{rr}}{\partial r} + \frac{1}{r} \frac{\partial \dot{S}_{\theta r}}{\partial \theta} + \frac{1}{r} \left(2\dot{S}_{rr} - \dot{S}_{\theta\theta} - \dot{S}_{\psi\psi} + \dot{S}_{\theta r} \cot \theta \right) &= 0, \\
 \frac{\partial \dot{S}_{r\theta}}{\partial r} + \frac{1}{r} \frac{\partial \dot{S}_{\theta\theta}}{\partial \theta} + \frac{1}{r} \left[\left(\dot{S}_{\theta\theta} - \dot{S}_{\psi\psi} \right) \cot \theta + 2\dot{S}_{r\theta} + \dot{S}_{\theta r} \right] &= 0,
 \end{aligned} \tag{S2}$$

and

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \dot{D}_r \right) + \frac{1}{r \sin \theta} \frac{\partial \left(\dot{D}_\theta \sin \theta \right)}{\partial \theta} = 0, \tag{S3}$$

respectively.

The incremental incompressibility constraint can be derived from Eq. (3.7) as

$$\frac{\partial \dot{u}_r}{\partial r} + \frac{1}{r} \left(\dot{u}_r + \frac{\partial \dot{u}_\theta}{\partial \theta} \right) + \frac{1}{r} (\dot{u}_r + \dot{u}_\theta \cot \theta) = 0. \quad (\text{S4})$$

We combine Eqs. (3.9) and (S4) to obtain

$$U'_r = -\frac{1}{r} (U_r + MU_\theta), \quad (\text{S5})$$

where the prime denotes the derivative with respect to r . From Eqs. (S1)_{4,7} and (S4) we get

$$U'_\theta = -\frac{1}{\alpha} \left[(S_{rr} - \alpha) \frac{M}{r} U_r + \frac{\alpha - S_{rr}}{r} U_\theta + \frac{\Gamma_{122} M}{K_{22} r} \Phi + \frac{1}{r} (r \Sigma_{r\theta}) \right]. \quad (\text{S6})$$

Substitution of Eq. (3.9) into Eq. (S1)₆ gives

$$\Phi' = \frac{2(\Gamma_{111} - \Gamma_{221})}{r} U_r - \frac{\Gamma_{111} - \Gamma_{221}}{r} M U_\theta - \frac{K_{11}}{r} (r \Delta_r). \quad (\text{S7})$$

Rewriting Eqs. (S1)₇, (S3) and (3.9) results in

$$(r \Delta_r)' = \frac{1}{r} \left[\frac{S_{rr} \Gamma_{22} M^2}{\alpha K_{22}} U_r + \frac{S_{rr} \Gamma_{22} M}{\alpha K_{22}} U_\theta - \left(\frac{1}{K_{22}} + \frac{\Gamma_{122}^2}{\alpha K_{22}^2} \right) M^2 \Phi - r \Delta_r - \frac{\Gamma_{122} M}{\alpha K_{22}} (r \Sigma_{r\theta}) \right]. \quad (\text{S8})$$

Then, we substitute Eq. (3.9) into Eqs. (S1)_{1,2,3,5,11} and (S2)₁ to get

$$(r \Sigma_{rr})' = \frac{1}{r} \left[\kappa_{11} U_r + \kappa_{12} U_\theta + \kappa_{13} (r \Delta_r) + r \Sigma_{rr} + \frac{(\alpha - S_{rr}) M}{\alpha} (r \Sigma_\theta) + \frac{S_{rr} \Gamma_{122} M^2}{\alpha K_{22}} \Phi \right]. \quad (\text{S9})$$

where

$$\kappa_{11} = 2(2A_{1111} - 4A_{1122} + A_{2222} + A_{2233} + 3\rho) + \frac{(\alpha - S_{rr})^2}{\alpha} M^2, \quad \kappa_{12} = \frac{(\alpha - S_{rr})^2}{\alpha}. \quad (\text{S10})$$

Similarly, from Eqs. (3.9), (S1)_{1,2,3,5} and (S2)₂, we have

$$(r \Sigma_{r\theta})' = \frac{1}{r} \left[\kappa_{21} U_r + \kappa_{22} U_\theta + \kappa_{13} U_z - M (r \Sigma_{rr}) - \frac{2\alpha - S_{rr}}{\alpha} (r \Sigma_{r\theta}) + \frac{S_{rr} K_{122} M}{\alpha K_{22}} \Phi \right]. \quad (\text{S11})$$

Finally we can write Eqs. (S5)-(S11) in the form (3.11).

$$\mathbf{G}_1 = \begin{bmatrix} -2 & M & 0 \\ -\frac{(\alpha - \sigma_{rr})M}{\alpha} & \frac{\alpha - \sigma_{rr}}{\alpha} & 0 \\ -\frac{\sigma_{rr}\beta M^2}{\alpha} & \frac{\sigma_{rr}\beta M}{\alpha} & -1 \end{bmatrix}, \quad \mathbf{G}_2 = \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{1}{\alpha} & \frac{\beta M}{\alpha} \\ 0 & -\frac{\beta M}{\alpha} & -\left(\frac{1}{K_{022}} + \frac{\beta^2}{\alpha} \right) M^2 \end{bmatrix}, \quad (\text{S12})$$

$$\mathbf{G}_3 = \begin{bmatrix} \kappa_{11} & \kappa_{12} & \kappa_{13} \\ \kappa_{21} & \kappa_{22} & \kappa_{23} \\ \kappa_{31} & \kappa_{32} & \kappa_{33} \end{bmatrix}, \quad \mathbf{G}_4 = \begin{bmatrix} 1 & \frac{(\alpha - \sigma_{rr})M}{\alpha} & -\frac{\sigma_{rr}\beta M^2}{\alpha} \\ -M & -\frac{2\alpha - \sigma_{rr}}{\alpha} & \frac{\sigma_{rr}\beta M}{\alpha} \\ 0 & 0 & 0 \end{bmatrix},$$

and

$$\begin{aligned}
A_{01212} - \frac{\Gamma_{0122}^2}{K_{022}} &= \alpha, & \frac{\Gamma_{0122}}{K_{022}} &= \beta, \\
A_{01221} + p - \frac{\Gamma_{0122}^2}{K_{022}} &= A_{01221} + A_{01212} - \sigma_{rr} - A_{01221} - \frac{\Gamma_{0122}^2}{K_{022}} = \alpha - \sigma_{rr} \\
\gamma_{21} &= A_{02121} - \frac{\Gamma_{0122}^2}{K_{022}}, \\
\kappa_{11} &= 2(2A_{01111} - 4A_{01122} + A_{02222} + A_{02233} + 3p) + M^2 \left(\gamma_{21} - \frac{(\alpha - \sigma_{rr})^2}{\alpha} \right), \\
\kappa_{12} = \kappa_{21} &= \left[\frac{(\alpha - \sigma_{rr})^2}{\alpha} - \gamma_{21} - (2A_{01111} - 4A_{01122} + A_{02222} + A_{02233} + 3p) \right] M, \\
\kappa_{22} &= - \left[M^2 (2A_{01122} - A_{01111} - A_{02222} - 2p) + (A_{02222} + p - A_{02233} - \gamma_{21}) + \frac{(\alpha - \sigma_{rr})^2}{\alpha} \right], \\
\kappa_{13} = -\kappa_{31} &= -2(\Gamma_{0111} - \Gamma_{0221}), \\
\kappa_{23} = -\kappa_{32} &= -(\Gamma_{0221} - \Gamma_{0111}) M, \\
\kappa_{33} &= -K_{011}.
\end{aligned} \tag{S13}$$

2 Incremental coefficients for a Gent material

From Eqs. (2.35) and (4.1), the radial stresses in the DE and elastic layers can be obtained as

$$\begin{aligned}
T_{rr}^d &= - \frac{\mu^d G^d}{2} \sum_{j=1}^6 \frac{2 \ln(\lambda - \eta_j^d) (\eta_j^d)^3 - \ln(\lambda - \eta_j^d) - 3 \ln(\lambda - \eta_j^d) \eta_j^d - G^d \ln(\lambda - \eta_j^d) \eta_j^d}{3 [(\eta_j^d)^3 - \eta_j^d] - G^d \eta_j^d} \Bigg|_{\lambda_i}^{\lambda} \\
&\quad + 2\mu^d G^d \ln \left(\frac{\lambda}{\lambda_i} \right) + \frac{\varepsilon}{2} \left(\frac{V r_m r_i}{r_i - r_m} \right)^2 \left(\frac{1}{r^4} - \frac{1}{r_i^4} \right) - P,
\end{aligned} \tag{S14}$$

and

$$\begin{aligned}
T_{rr}^e &= \frac{\mu^e G^e}{2} \sum_{j=1}^6 \frac{2 \ln(\lambda - \eta_j^e) (\eta_j^e)^3 - \ln(\lambda - \eta_j^e) - 3 \ln(\lambda - \eta_j^e) \eta_j^e - G^e \ln(\lambda - \eta_j^e) \eta_j^e}{3 [(\eta_j^e)^3 - \eta_j^e] - G^e \eta_j^e} \Bigg|_{\lambda}^{\lambda_o} \\
&\quad - 2\mu^e G^e \ln \left(\frac{\lambda_o}{\lambda} \right),
\end{aligned} \tag{S15}$$

respectively, where η_j^s ($s = d, e$; $j = 1 - 6$) are the six roots of the polynomial equation $1 - (3 + G^s)(\eta^s)^4 + 2(\eta^s)^6 = 0$.

Further, the circumferential stresses in the balloon can be obtained from Eq. (2.37) as

$$T_{\theta\theta}^d = T_{rr}^d - \frac{G^d \mu^d}{G^d - (\lambda^{-4} + 2\lambda^2 - 3)} (\lambda^{-4} - \lambda^2) - \varepsilon \left[\frac{V r_i r_m}{r^2 (r_m - r_i)} \right]^2 \tag{S16}$$

at the DE layer, and

$$T_{\theta\theta}^e = T_{rr}^e - \frac{G^e \mu^e}{G^e - (\lambda^{-4} + 2\lambda^2 - 3)} (\lambda^{-4} - \lambda^2) \tag{S17}$$

at the elastic layer, respectively.

As a result, the deformation of the solid can be solved using the interfacial condition

$$T_{rr}^e(r_m) = T_{rr}^d(r_m). \tag{S18}$$

We note that the displacements and normal stresses at the interfacial face of the layers are continuous, but there will be a jump for the circumferential stresses at the interface [1].

The non-zero components of the tensors containing the electro-elastic moduli for the considered

Gent elastomer (with the superscript s omitted) read

$$\begin{aligned}
A_{1111} &= \frac{\mu G [1 + \lambda^4(G + 3) - 2\lambda^6]}{[1 - \lambda^4(G + 3) + 2\lambda^6]^2} + \varepsilon D_r^2, & A_{1122} = A_{1133} &= \frac{2\mu G \lambda^6}{[1 - \lambda^4(G + 3) + 2\lambda^6]^2}, \\
A_{1212} = A_{1313} &= -\frac{\mu G}{1 - \lambda^4(G + 3) + 2\lambda^6} + \varepsilon D_r^2, \\
A_{2121} = A_{3131} = A_{2323} = A_{3232} &= -\frac{\mu G \lambda^6}{1 - \lambda^4(G + 3) + 2\lambda^6}, & (S19) \\
A_{2222} = A_{3333} &= \frac{\mu G \lambda^6 [\lambda^4(G + 3) - 1]}{[1 - \lambda^4(G + 3) + 2\lambda^6]^2}, & A_{2233} &= \frac{2\mu G \lambda^{12}}{[1 - \lambda^4(G + 3) + 2\lambda^6]^2}, \\
\Gamma_{111} = 2\Gamma_{122} = 2\Gamma_{212} = 2\Gamma_{133} = 2\Gamma_{313} &= 2\varepsilon D_r, & K_{11} = K_{22} = K_{33} &= \varepsilon.
\end{aligned}$$

References

- [1] S. Roccabianca, M. Gei, and D. Bigoni. Plane strain bifurcations of elastic layered structures subject to finite bending: theory versus experiments. *IMA Journal of Applied Mathematics*, 75(4):525–548, 2010.