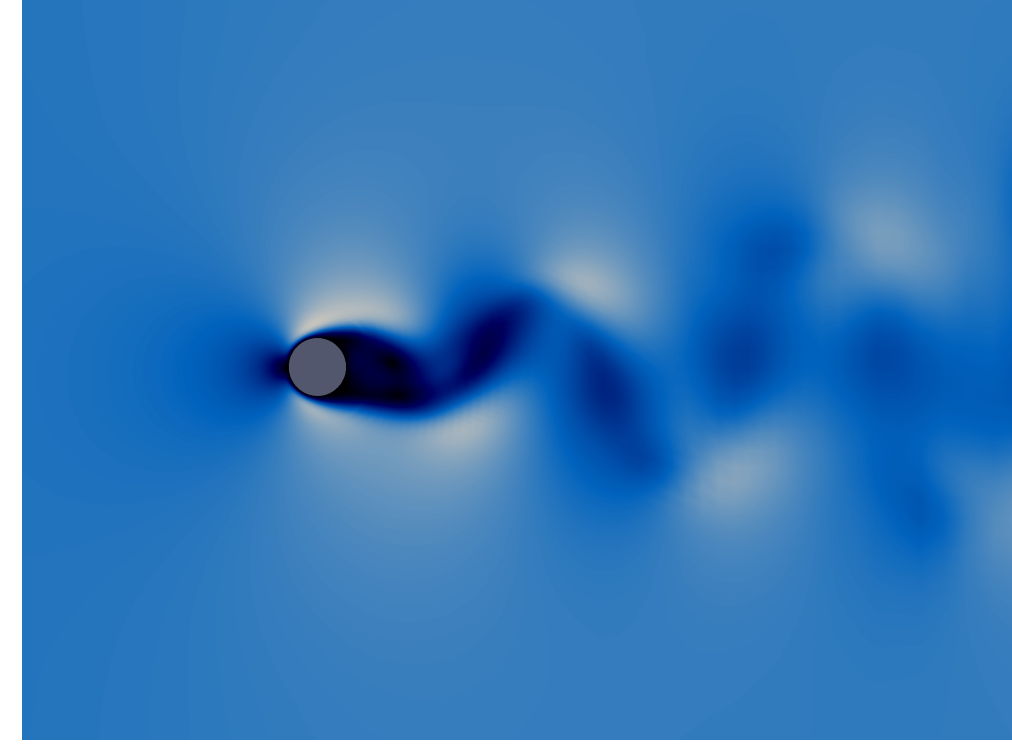


Introduction - 1

Motivations

- **Vortex-induced vibration** is a well known phenomenon in many engineering fields and a reliable ROM is still missing in literature.
- There are interesting non-linear phenomena particularly challenging to be reproduced with a ROM.
- For design purposes several configurations need to be tested and a reliable ROM would dramatically **reduce the computational time**.



Methodology-Overview

Development of reduced order methods for the analysis of **vortex shedding** phenomena around a circular cylinder. The reduction has been performed using the following numerical techniques:

- High Fidelity simulation of the physical problem through the **finite volume** solver **OpenFOAM®** [4]. (**BOX 2**)
- Collection of the **snapshots** and construction of the reduced basis space \mathbb{V}_{rb} using a **POD** [1] approach. (**BOX 3**)
- Projection of the unsteady Navier-Stokes equation onto the reduced basis space \mathbb{V}_{rb} in order to construct the **POD-Galerkin dynamical system**. [2]. (**BOX 4**)

Construction of \mathbb{V}_{rb} - 3

Assumption: reduced order solution for the velocity, pressure and fluxes fields is given by a linear combination of the **bases functions** $\varphi_i(\mathbf{x})$ (which depends only on space) multiplied by a **temporal coefficients** $a_i(t)$:

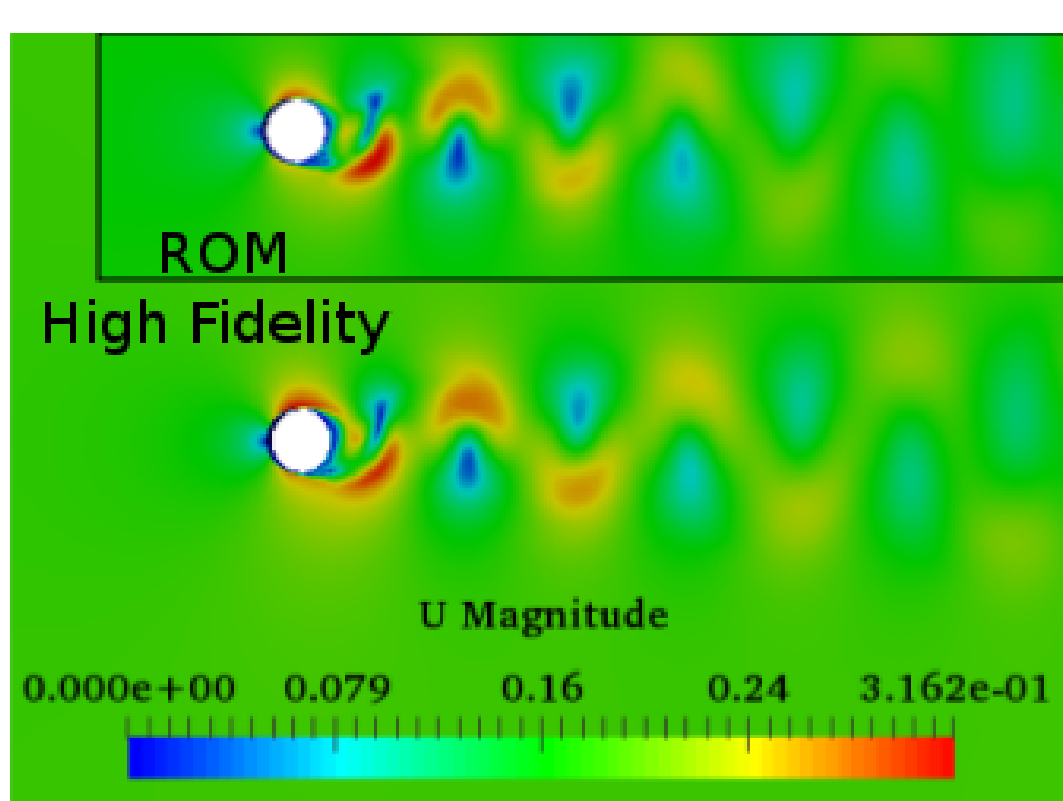
$$\mathbf{u}(\mathbf{x}, t) \approx \mathbf{u}_r(\mathbf{x}, t) = \sum_{i=1}^{N_r} a_i(t) \varphi_i(\mathbf{x})$$

The reduced basis space $\mathbb{V}_{rb} = \text{span}(\varphi_i)$ is constructed solving the following minimization problem:

$$\mathbb{V}_{rb} = \arg \min \frac{1}{N_s} \sum_{n=1}^{N_s} \|\mathbf{u}_n(\mathbf{x}) - \sum_{i=1}^{N_r} \langle \mathbf{u}_n(\mathbf{x}), \varphi_i(\mathbf{x}) \rangle_{L^2} \varphi_i(\mathbf{x})\|_{L^2}^2$$

Where $\mathbf{u}_n(\mathbf{x}, t, u_{in})$ are field solutions (Snapshots) sampled at different inlet velocities and times.

Results - 5



Comparison between velocity fields at $Re=6000$ with 20 modes. At the top is the reduced basis case lower at the bottom is the high fidelity one.

The error in L^2 -norm for the ROM lift coefficient, $Re = 100$ for different number of modes used.

Number of modes	Relative Error
2	1.0014363
3	0.0685620
5	0.0886061
8	0.0660731
10	0.0054784
13	0.0040657

High Fidelity problem - 2

Governing Equations

The physical problem is modelled using the **unsteady incompressible Navier-Stokes equations**. For low values of the Reynolds number the following system of equations is considered:

$$\begin{cases} \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} - \nu \nabla^2 \mathbf{u} + \nabla p = 0 \\ \nabla \cdot \mathbf{u} = 0 \end{cases} \quad \text{in } \Omega$$

while for higher values of the Reynolds number a **URANS** approach with a $k - \omega$ [3] **turbulence modelling** is used:

$$\begin{cases} \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = \nabla \cdot \left[-p\mathbf{I} + (\nu + \nu_t) (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) - \frac{2}{3} k \mathbf{I} \right] \\ \nabla \cdot \mathbf{u} = 0 \\ \nu_t = f(k, \omega) \\ \text{Transport-Diffusion equation for } k \\ \text{Transport-Diffusion equation for } \omega \end{cases} \quad \text{in } \Omega$$

The space discretization of the equations has been performed using a **finite volume** approach

The POD-Galerkin Dynamical system - 4

Laminar Case

Using a **finite volume discretization** it appears inside the discretized equation also the **mass fluxes** over the faces of the cells. It is then made the assumption that the velocity field, the mass flux field and the pressure field can be decomposed as:

$$\begin{pmatrix} \mathbf{u}(\mathbf{x}, t) \\ F(\mathbf{x}, t) \\ p(\mathbf{x}, t) \end{pmatrix} \approx \begin{pmatrix} \mathbf{u}_r(\mathbf{x}, t) \\ F_r(\mathbf{x}, t) \\ p_r(\mathbf{x}, t) \end{pmatrix} = \sum_{i=1}^{N_r} a_i(t) \begin{pmatrix} \varphi_i(\mathbf{x}) \\ \psi_i(\mathbf{x}) \\ \chi_i(\mathbf{x}) \end{pmatrix}$$

The governing equations are then **projected** onto the spatial bases and the original fields are replaced with the approximated fields. This operation generates the **POD-Galerkin system**:

$$\frac{da_i(t)}{dt} = \nu \sum_{i=1}^{N_r} B_{ji} a_i(t) - \sum_{k=1}^{N_r} \sum_{i=1}^{N_r} C_{jki} a_k(t) a_i(t) - \sum_{i=1}^{N_r} A_{ji} a_i(t)$$

Where B , C and A read:

$$B_{ji} = (\varphi_j, \Delta \varphi_i)_{L^2}; \quad C_{jki} = (\varphi_j, \nabla \cdot (\psi_k \varphi_i))_{L^2}; \quad A_{ji} = (\varphi_j, \nabla \chi_i)_{L^2}$$

and the dynamical system can be rewritten as:

$$\dot{\mathbf{a}} = \nu \mathbf{B} \mathbf{a} - \mathbf{a}^T \mathbf{C} \mathbf{a} - \mathbf{A} \mathbf{a}$$

Turbulent Case

For the turbulent the approximated **eddy viscosity** is written as:

$$\nu_t(\mathbf{x}, t) \approx \nu_{t,r}(\mathbf{x}, t) = \sum_{i=1}^{N_r} a_i(t) \phi_i(\mathbf{x})$$

that leads to the following dynamical system:

$$\dot{\mathbf{a}} = \nu (\mathbf{B} + \mathbf{B} \mathbf{T}) \mathbf{a} - \mathbf{a}^T (\mathbf{C} - \mathbf{C} \mathbf{T}_1 - \mathbf{C} \mathbf{T}_2) \mathbf{a} - \mathbf{A} \mathbf{a} + \tau (\mathbf{u}_{bc} \mathbf{D} - \mathbf{E} \mathbf{a})$$

where it is introduced also the effect of different **inlet velocities** \mathbf{u}_{BC} with a **penalization factor** τ . The additional terms are still obtained with Galerkin projection onto \mathbb{V}_{rb} and read:

$$D_j = \langle \varphi_j \rangle_{L^2, \partial \Omega}; \quad E_{ji} = \langle \varphi_j, \varphi_i \rangle_{L^2, \partial \Omega}; \quad B T_{ji} = \langle \varphi_j, \nabla \cdot (\nabla \varphi_i^T) \rangle_{L^2}$$

$$C T_{1jki} = \langle \varphi_j, \phi_k \Delta \varphi_i \rangle_{L^2}; \quad C T_{2jki} = \langle \varphi_j, \nabla \cdot \phi_k (\nabla \varphi_i^T) \rangle_{L^2}$$

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